

①

Løsningsforslag

FY 1005 / TFY 4165

22.05.2015, 09.00-13.00

Oppg 1

a	:	A
b	:	D
c	:	C
d	:	A
e	:	D
f	:	D
g	:	C
h	:	C

2

Oppgave 2

a)

$$Z = \sum_{\text{tilstand}} e^{-\beta E(\text{tilstand})}$$

$$= (Z_1)^N$$

Hvilken faktor $1/N!$ utelukkes, slik at vi betrakter partiklene som klassiske og ikke ombyttbare (de kan f.eks. sitte fast i rommet)

$$\underline{Z_1 = e^{-\beta \epsilon_1} + e^{-\beta \epsilon_2} + e^{-\beta \epsilon_3}}$$

$$\epsilon_1 = 0 \quad ; \quad \epsilon_2 = \epsilon \quad ; \quad \epsilon_3 = -\epsilon$$

$$Z = (Z_1)^N$$

$$Z_1 = 1 + e^{-\beta \epsilon} + e^{-\beta(-\epsilon)}$$

$$= 1 + e^{\beta \epsilon} + e^{-\beta \epsilon}$$

$$\underline{= 1 + 2 \cosh(\beta \epsilon)}$$

$$\underline{b)} \quad \langle \varepsilon \rangle = - \frac{\partial}{\partial \beta} (\ln(Z_1)) \quad (3)$$

$$= - \frac{\partial}{\partial \beta} \ln(1 + 2 \cosh(\beta \varepsilon))$$

$$= - \frac{1}{1 + 2 \cosh(\beta \varepsilon)} \cdot 2 \varepsilon \sinh(\beta \varepsilon)$$

$$= \underline{\underline{- \frac{2 \varepsilon \sinh(\beta \varepsilon)}{1 + 2 \cosh(\beta \varepsilon)}}}$$

$$\beta \rightarrow 0:$$

$$\cosh(\beta \varepsilon) \approx 1$$

$$\sinh(\beta \varepsilon) \approx \beta \varepsilon$$

$$\langle \varepsilon \rangle \approx \underline{\underline{- \frac{2}{3} \beta \varepsilon^2 \rightarrow 0}}$$

Partiklere
fordelt likt
på alle tre
niveauer.

$$\beta \rightarrow \infty:$$

$$\langle \varepsilon \rangle \approx - \frac{2 \varepsilon \sinh(\beta \varepsilon)}{2 \cosh(\beta \varepsilon)}$$

$$= - \varepsilon \tanh(\beta \varepsilon) \approx \underline{\underline{- \varepsilon}}$$

Alle partikler
i laveste
niva

$$c) \quad C_V = \left(\frac{\partial u}{\partial T} \right)_V$$

(4)

$$= - \frac{\partial}{\partial T} \left(\frac{2\varepsilon \sinh(\beta\varepsilon)}{1 + 2 \cosh(\beta\varepsilon)} \right)$$

$$= - \frac{\partial}{\partial \beta} \left(\frac{\quad}{\quad} \right) \frac{\partial \beta}{\partial T}$$

$$= \frac{1}{k_B T^2} \frac{\partial}{\partial \beta} \left(\frac{\quad}{\quad} \right)$$

$$= k_B \beta^2 \frac{\partial}{\partial \beta} \left(\frac{\quad}{\quad} \right)$$

$$\frac{\partial}{\partial \beta} \left(\frac{\quad}{\quad} \right) = 2\varepsilon \left\{ \frac{\varepsilon \cosh(\beta\varepsilon)}{1 + 2 \cosh(\beta\varepsilon)} \right.$$

$$\left. - \frac{\sinh(\beta\varepsilon)}{(1 + 2 \cosh(\beta\varepsilon))^2} \cdot 2\varepsilon \sinh(\beta\varepsilon) \right\}$$

$$= 2\varepsilon^2 \frac{\quad}{(1 + 2 \cosh(\beta\varepsilon))^2} \left\{ \cosh(\beta\varepsilon) + 2 \cosh^2(\beta\varepsilon) - 2 \sinh^2(\beta\varepsilon) \right\}$$

$$= \frac{2\varepsilon^2}{(1 + 2 \cosh(\beta\varepsilon))^2} (2 + \cosh(\beta\varepsilon))$$

5

$$C_v = 2 \frac{\epsilon^2 \beta^2 k_B (2 + \cosh(\beta \epsilon))}{(1 + 2 \cosh(\beta \epsilon))^2}$$
$$= 2 k_B \left(\frac{\epsilon}{k_B T} \right)^2 \left(\frac{2 + \cosh(\beta \epsilon)}{(1 + 2 \cosh(\beta \epsilon))^2} \right)$$

$$\beta \rightarrow \infty$$

$$C_v \approx 2 (\beta \epsilon)^2 k_B \frac{1}{2} \frac{e^{-\beta \epsilon}}{e^{2\beta \epsilon}}$$

$$= k_B (\beta \epsilon)^2 e^{-\beta \epsilon} \xrightarrow{\beta \rightarrow \infty} 0$$

$$\beta \rightarrow \infty \quad (T \rightarrow 0):$$

Alle partikler sanket i laveste energi-nivå, dvs grundtilstanden. Her er der ingen energi-fluktuationer; grundtilstanden har ingen bevægelse i lavere varme.

Varmekapaciteten forsvinder dermed ved lave temperaturer.

$\beta \rightarrow 0 \quad (T \rightarrow \infty):$

(6)

$$C_V \approx 2 (\beta \epsilon)^2 k_B \frac{3}{9} = \frac{2}{3} k_B (\beta \epsilon)^2 \rightarrow 0$$

Resultatet i høytemperaturregionen er ikke det man ville fått fra $f \neq 0$ kvadratiske frihetsgrader

~~1~~
I dette tilfellet er $f=0$,
ingen kvadratiske frihetsgrader
i systemet

$$C_V = f \cdot \frac{1}{2} k_B$$

$$f=0 : \quad \underline{C_V = 0}$$

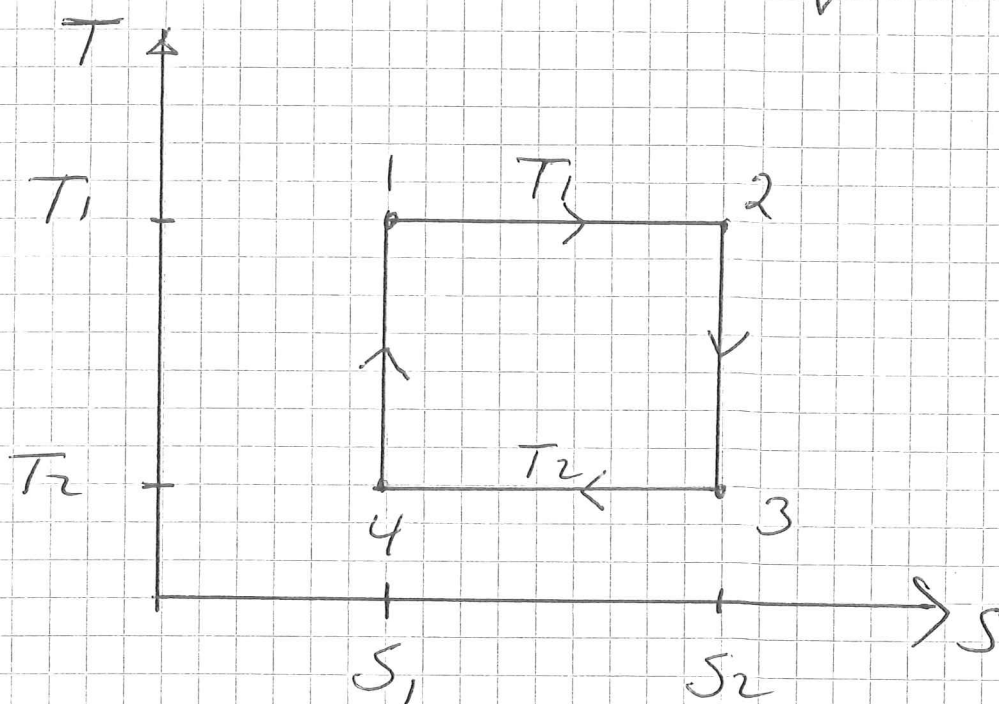
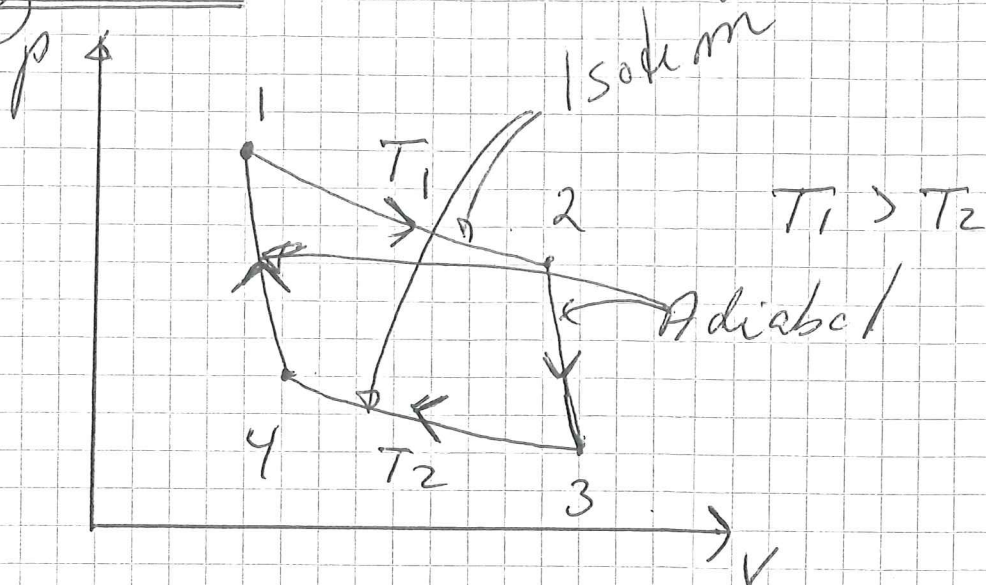
Svaret er i overensstemmelse
med ekvipartisjonsprinsippet.

Oppgave 3

Carnot-process

(7)

a)



b) Tilført varme : Q_1 (T_1)
Avgitt varme : Q_2 (T_2)

$$\Delta Q = T \Delta S = \Delta U + p \Delta V$$

$$Q_1 = T_1 \Delta S \quad (\Delta S = S_2 - S_1)$$

$$Q_2 = -T_2 \Delta S$$

$$\eta = \frac{W}{Q_1} = \frac{Q_1 - |Q_2|}{Q_1} = \frac{\Delta S (T_1 - T_2)}{\Delta S T_1}$$

$$\eta = 1 - \frac{T_2}{T_1}$$

$$\Delta S = S_2 - S_1 = \int_{V_1}^{V_2} \left(\frac{\partial S}{\partial V} \right)_T dV$$

Karakteristikkene helt ut av η .
Kommentar:

$$T dS = dU + p dV$$

$$dS = \frac{1}{T} \left(\left(\frac{\partial U}{\partial T} \right)_V dT + \left(\frac{\partial U}{\partial V} \right)_T dV \right) + \frac{p}{T} dV$$

$$dT = 0$$

$$dS = \frac{1}{T} \left(p + \left(\frac{\partial U}{\partial V} \right)_T \right) dV$$

$$\Delta S = \frac{1}{T_1} \int_{V_1}^{V_2} \left(p + \left(\frac{\partial U}{\partial V} \right)_{T=T_1} \right) dV$$

$$= \frac{1}{T_2} \int_{V_3}^{V_4} \left(p + \left(\frac{\partial U}{\partial V} \right)_{T=T_2} \right) dV$$

ΔS inneholder all info om tilstandsligning og termodyn. til arbeidsprosedyrene, men karakteristikkene helt ut av η .

c

1 → 2: Isotherm

(9)

$$du = \left(\frac{\partial u}{\partial T} \right)_V dT + \left(\frac{\partial u}{\partial V} \right)_T dV$$

$$\left. \begin{array}{l} dT = 0 \\ \left(\frac{\partial u}{\partial V} \right)_T = 0 \end{array} \right\} \underline{\underline{\Delta u = u(2) - u(1) = 0}}$$

$$\Delta S = \frac{1}{T_1} \int_{V_1}^{V_2} p dV$$

$$pV = Nk_B T$$

$$\Delta S = Nk_B \frac{T_1}{T_1} \int_{V_1}^{V_2} \frac{dV}{V}$$

$$= Nk_B \ln \left(\frac{V_2}{V_1} \right)$$

$$\left(\Delta S = \frac{1}{T_2} \int_{V_3}^{V_4} p dV \right)$$
$$= Nk_B \ln \left(\frac{V_3}{V_4} \right)$$

$$\left(\frac{V_3}{V_4} = \frac{V_2}{V_1} \right)$$

$$\Delta F = \Delta U - T_1 \Delta S$$

$$= 0 - Nk_B T_1 \ln \left(\frac{V_2}{V_1} \right)$$

$$= -Nk_B T_1 \ln \left(\frac{V_2}{V_1} \right)$$

$$V_2 > V_1 \Rightarrow \Delta F = F(2) - F(1) < 0$$

Tilstand 2 har lavest fri energi (størst entropi)

Oppgave 4

a) $\langle v \rangle$

2D. fartfordeling

$$F_{2D}(v) dv = 2\pi v dv \left(\frac{m}{2\pi k_B T} \right) e^{-\alpha v^2}$$

$$= \frac{m}{2k_B T} (v_x^2 + v_y^2)$$

$$\langle v \rangle = \frac{2\pi m}{2\pi k_B T} \int_0^\infty dv v^2 e^{-\alpha v^2}$$

$$\alpha = \frac{m}{2k_B T} \equiv I$$

$$I = \int_0^\infty dx^2 e^{-\alpha x^2} =$$

$$= -\frac{1}{2\alpha} \sqrt{\frac{\pi}{\alpha}}$$

$$I = \frac{1}{4} \frac{\sqrt{\pi}}{\alpha^{3/2}}$$

(11)

$$\langle v \rangle = 2\alpha \frac{\sqrt{\pi}}{4\alpha^{3/2}}$$

$$= \frac{\sqrt{\pi}}{4\alpha} = \frac{\sqrt{2\pi k_B T}}{4m}$$

$$= \frac{\sqrt{\pi k_B T}}{2m}$$

$$\langle v^2 \rangle = \langle v_x^2 \rangle + \langle v_y^2 \rangle + \langle v_z^2 \rangle = 3 \langle v^2 \rangle$$

$$\langle v^2 \rangle = \frac{m}{2\pi k_B T} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} v^2 e^{-\alpha v^2} dv_x dv_y dv_z$$

$$= \frac{2\pi m}{2\pi k_B T} \int_0^{\infty} dv v^3 e^{-\alpha v^2}$$

$$x = \alpha v^2$$

$$v = \frac{1}{\sqrt{\alpha}} dx$$

$$\langle v^2 \rangle = \frac{m}{k_B T} \frac{1}{\alpha^2} \int_0^{\infty} dx x^3 e^{-x^2}$$

$$z = x^2 \quad dx x^3 = \frac{1}{4} dx^4$$

$$dx x^3 = \frac{1}{2} z dz$$

$$\langle v^2 \rangle = \frac{m}{k_B T} \frac{1}{\alpha^2} \frac{1}{2} \int_0^\infty dz z e^{-z} \quad (12)$$

$$I = \int_0^\infty dz z e^{-z} = \int_0^\infty dz z e^{-\alpha z} \Big|_{\alpha=1}$$

$$= - \frac{d}{d\alpha} \int_0^\infty dz e^{-\alpha z} \Big|_{\alpha=1} = - \frac{d}{d\alpha} \left(\frac{1}{\alpha} \right) = \frac{1}{\alpha^2} \Big|_{\alpha=1}$$

$$\underline{I = 1} \quad \Rightarrow$$

$$\langle v^2 \rangle = \frac{1}{2} \frac{2\alpha}{\alpha^2} = \frac{1}{\alpha} = \underline{\underline{\frac{2k_B T}{m}}}$$

(Kunne også gjøres:

$$\frac{1}{2} m \langle v^2 \rangle = \frac{1}{2} m \langle v^2 \rangle = 2 \cdot \frac{1}{2} k_B T$$

v_x^2, v_y^2

$$\langle v^2 \rangle = \frac{2k_B T}{m}$$

Vi har:

$$\langle v^2 \rangle - \langle v \rangle^2 = \frac{k_B T}{m} \left(2 - \frac{\pi}{2} \right) > 0$$

Det er så vi forventer:

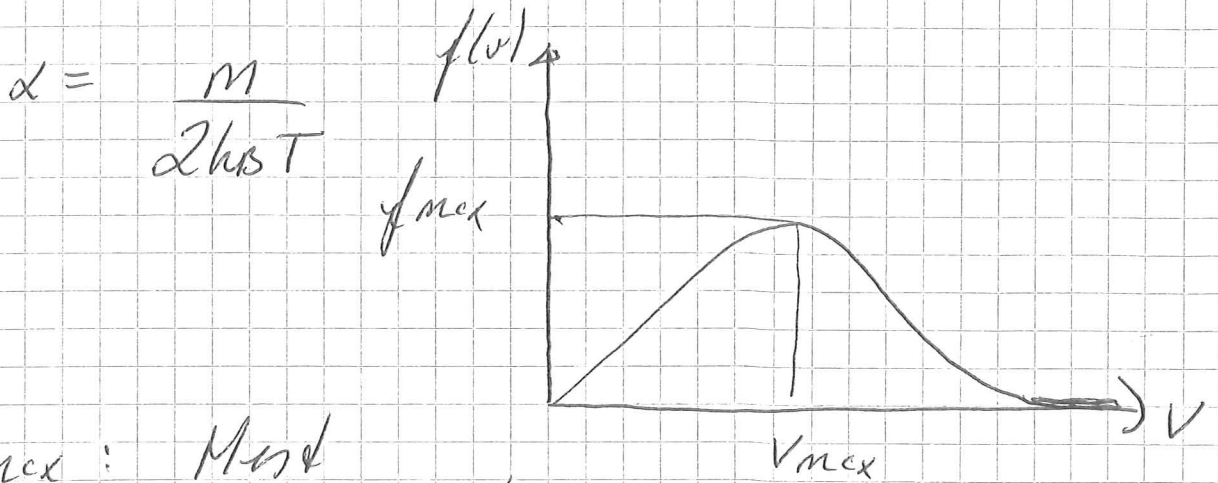
$$\langle v^2 \rangle - \langle v \rangle^2 = \underline{\underline{\langle (v - \langle v \rangle)^2 \rangle}} > 0$$

b) Fartfordelinger:

$$f(v) dv = \frac{m}{2k_B T} \cdot 2\pi v dv e^{-\frac{m}{2k_B T} v^2}$$

$$f(v) = 2\pi \frac{m}{2k_B T} v e^{-\alpha v^2}$$

$$= C v e^{-\alpha v^2}$$



v_{max} : Most sannsynlige farten

Finnes ved:

$$\frac{df}{dv} = 0$$

$$C (e^{-\alpha v^2} - 2\alpha v^2 e^{-\alpha v^2}) = 0$$

$$1 - 2\alpha v^2 = 0$$

$$v_{max} = \sqrt{\frac{1}{2\alpha}} = \sqrt{\frac{k_B T}{m}}$$

$$v_{max} = \sqrt{\frac{1.38 \cdot 10^{-23} \cdot 300}{2.325 \cdot 10^{-26}}}$$

14

$$= \underline{\underline{422 \text{ m/s}}}$$

c) Midlere inputs:

$$\langle p_x \rangle = m \langle v_x \rangle$$

$$\langle v_x \rangle = \sqrt{\frac{m}{2\pi k_B T}} \int_{-\infty}^{\infty} dv_x v_x e^{-\frac{m}{2k_B T} v_x^2}$$

$$= 0$$

$$\underline{\underline{\langle p_x \rangle = 0}}$$

Midlere kinetisk energi:

$$\frac{1}{2} m \langle v_x^2 \rangle = \frac{1}{2} k_B T \quad (\text{Ekwipartitionsprincippet})$$

$$\langle v_x^2 \rangle = \frac{k_B T}{m}$$

Alternativt:

$$\langle v_x^2 \rangle = \sqrt{\frac{m}{2\pi k_B T}} \int_{-\infty}^{\infty} dv_x v_x^2 e^{-\alpha v_x^2}$$

$$\alpha = \frac{m}{2k_B T}$$

$$\frac{1}{2} \frac{\sqrt{\pi}}{\alpha^{3/2}}$$

$$\langle v_x^2 \rangle = \sqrt{\frac{m}{2\pi h \omega T}} \cdot \frac{1}{2} \sqrt{\pi} \frac{2 h \omega T}{m} \sqrt{\frac{2 h \omega T}{m}} \quad (15)$$

$$= \sqrt{\frac{m}{2\pi h \omega T}} \sqrt{\frac{2\pi h \omega T}{m}} \frac{1}{2} \frac{2 h \omega T}{m}$$

$$= \frac{h \omega T}{m}$$

$$\underline{\underline{\frac{1}{2} m \langle v_x^2 \rangle = \frac{1}{2} h \omega T}}$$