

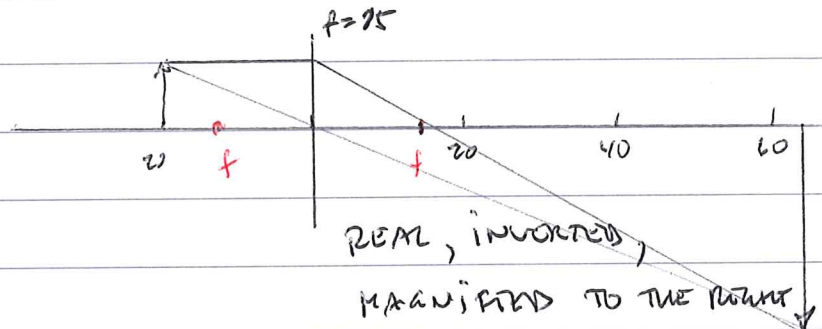
LF EXAM TFY4195 M2020 (5. DEC, 2020)

MC 8 $E = h\nu = \frac{hc}{\lambda} = \frac{6.62 \cdot 10^{-34} \cdot 3 \cdot 10^8}{10^{-10}}$ $[J] = \frac{\text{kg} \cdot \text{m}^2 / \text{s}^2 \cdot \text{m}}{\text{m}}$

CHANGE TO eV $E = q \cdot U$ $\Rightarrow E(\text{eV}) = \frac{6.62 \cdot 10^{-34} \cdot 3 \cdot 10^8}{10^{-10} \cdot 1.6 \cdot 10^{-19}} = 12400 \text{ eV} = \underline{12.4 \text{ keV}}$
 CHANGE \uparrow TELECOM VOLT

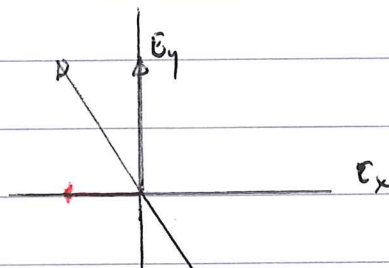
MC 7 $s_0 = 20 \text{ cm}$ $\frac{1}{20} + \frac{1}{s_i} = \frac{1}{15} \Rightarrow \frac{1}{s_i} = \frac{1}{15} - \frac{1}{20} = \frac{1}{60} \Rightarrow s_i = 60$

$M_T = -\frac{s_i}{s_0} = -3$



MC 10 $E_x = 4.6 \cos(kz - \omega t)$
 $E_y = 4.6 \sin(kz - \omega t)$ $\frac{\pi}{2}$ PHASE-SHIFT, SAME AMPLITUDE \Rightarrow CIRCULAR

$E_x = 2.2 \cos(kz - \omega t + \pi)$
 $E_y = 4.6 \cos(kz - \omega t)$



$E_x = 2.2 \cos(kz - \omega t + \frac{\pi}{4})$
 $E_y = 2.2 \cos(kz - \omega t - \frac{\pi}{4})$

$\frac{\pi}{2}$ PHASE-SHIFT DIFFERENCE, SAME AMPLITUDE \Rightarrow CIRCULAR

$E_x = 4.6 \cos(kz - \omega t - \frac{\pi}{2})$

$E_y = 4.6 \sin(kz - \omega t)$

$\sin \alpha = \cos(\alpha - \frac{\pi}{2})$

LINEAR 45°

THE REMAINING 2 HAVE DIFFERENT AMPLITUDES, PHASE-DIFFERENCES $\neq 0$ & π
 \Rightarrow ELLIPTICALLY POLARIZED

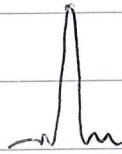
MCL WE CAN SOLVE THIS BY EXCLUSION PRINCIPLE



THESE SEPARATIONS ARE GIVEN BY THE (NUMBER N) SEPARATION OF SLITS.

THIS WIDTH IS GIVEN BY SLIT WIDTH " b "

3) CENTER



THIS HAS THE MOST NARROW DIFFRACTION PATTERN \rightarrow WIDEST SLIT (SINGLE SLIT 0.1 mm WIDE)

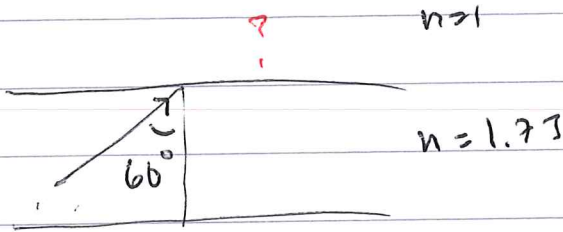
- 4) $\left\{ \begin{array}{l} \text{TYPICAL MULTI-SLIT, 6 SLITS 0.025 mm WIDE SEPARATED 0.1 mm ONLY} \\ \text{MUST HAVE THE SAME / SIMILAR } b \end{array} \right.$ ALTERNATIVE
- 5) \leftarrow TYPICAL SINGLE SLIT 0.025 mm

- 1) } BOTH HAS BROADER ENVELOPE \Rightarrow 0.01 mm WIDE
- 2) }

1) HAS LARGER WIDTH BETWEEN PEAKS \Rightarrow SMALLEST SLIT SEPARATION 0.03

MC 5

INTERNAL REFLECTION



$$1.75 \cdot \sin 60^\circ = 1 \cdot \sin \alpha$$

$$1.499 > 1$$

TOTAL INTERNAL REFLECTION

All light is REFLECTED

MC 11

THE GRATING EQUATION

LET $\lambda = 550 \text{ nm}$

$$a \cdot \sin \theta = m \cdot \lambda$$

↓ PROOF

GRATING G1

$$a_1 = 2.5 \cdot 10^{-6}$$

$$\Rightarrow \sin \theta_1 = \frac{2.550 \text{ nm}}{2.5 \cdot 10^{-6}} \Rightarrow \theta_1 = 26.10^\circ$$

GRATING G2

$$a_2 = 2 \cdot a_1 = 5 \cdot 10^{-6}$$

$$\theta_2 = 12.71^\circ$$

STATEMENT A)

ANGULAR DISPERSION = $\frac{m}{a \cos \theta}$

$$\theta_1 \rightarrow 8.91 \cdot 10^{-4} \frac{\text{rad}}{\text{nm}}$$

SO DISPERSION IS SMALLER
FOR G2

$$\theta_2 \rightarrow 4.10 \cdot 10^{-4} \frac{\text{rad}}{\text{nm}}$$

STATEMENT B)

RESOLUTION POWER $R = \frac{\lambda}{(\Delta\lambda)_{\text{min}}} = m \cdot N$

SINCE GRATING 2 HAS HALF THE NUMBER

$$\Rightarrow R_{G1} > R_{G2}$$

G1

MC 13

$$\begin{pmatrix} 2 & -14 \\ 1/2 & -3 \end{pmatrix} \begin{pmatrix} 1 & s_0 \\ 0 & 1 \end{pmatrix} =$$

$f_i \rightarrow$ IMAGE OBJECT $\rightarrow f_o$

$$= \begin{pmatrix} 2 & 2s_0 - 14 \\ 1/2 & s_0/2 - 3 \end{pmatrix}$$

$= 0$ GIVES IMAGING
CONDITION

$$s_0 = 7 \text{ cm}$$

M_T $M_T = 2$ REAL, MAGNIFIED, UPRIGHT IMAGE

MC 14

WE RELATE THE GUIDED WAVE \rightarrow ASSUMED

TO BE PROPORTIONAL TO

$$e^{i(\beta z - \omega t)}$$

WITH $\beta = \frac{2\pi}{\lambda} \cdot N$; THE k -VECTOR FOR THE GUIDED MODE
 \uparrow EFFECTIVE INDEX

ALSO $N_{TM} < N_{TE}$ FOR ISOTROPIC SYSTEMS

$$\text{AS } v_{ph} = \frac{c}{n} \Rightarrow v_{TM} > v_{TE}$$

$$\text{ALSO } v_{ph} = \frac{3 \cdot 10^8}{N} \sim 2 \cdot 10^8 \frac{\text{m}}{\text{s}}$$

$N \approx 1.485$ FROM FIGURE

MC9

$n = 1.5$

LENSMAKER FORMULA

$R_1 = 15 \text{ cm}$

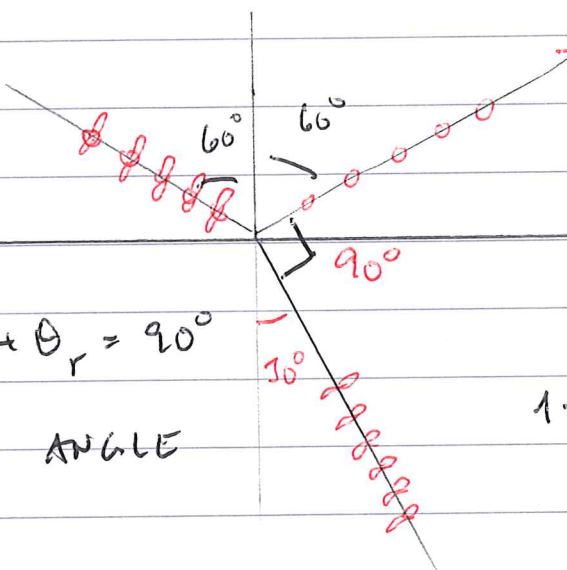
$R_2 = 10 \text{ cm}$

$$\frac{1}{f} = (n-1) \left(\frac{1}{R_1} + \frac{1}{R_2} \right)$$

↑
SIGN CONVENTION FOR TWO CONVEX SURFACES

$$\frac{1}{f} = 0.5 \left(\frac{1}{15} + \frac{1}{10} \right) = \frac{1}{12} \Rightarrow \underline{f = 12 \text{ cm}}$$

MC4



NO REFLECTED TM LIGHT @ BREWSTER ANGLE

$n = 1$

$n = 1.77$

SINCE $\theta_i + \theta_r = 90^\circ$

BREWSTER ANGLE

$$1 \cdot \sin 60^\circ = 1.77 \cdot \sin \alpha$$

$$0.5006 = \sin \alpha \Rightarrow \alpha = 30.0^\circ$$

TRANSMISSION LIGHT IS MOSTLY POLARIZED IN THE PLANE OF INCIDENCE

MC2

THE CORRELATION LENGTH CAN BE WRITTEN

$$L_c = \frac{\lambda^2}{\Delta\lambda} = \frac{500^2}{10} = 30.25 \cdot 10^3 \text{ nm} \sim 30 \mu\text{m}$$

MC12

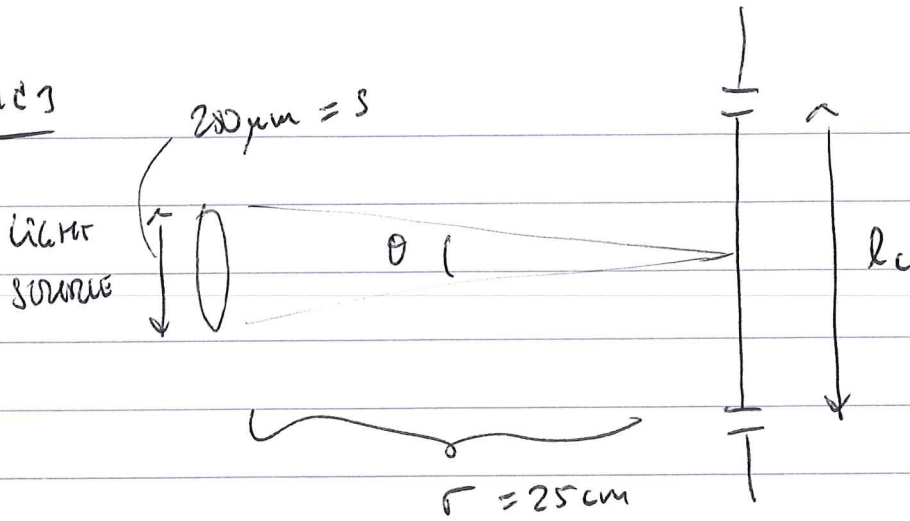
$$M_{12} = \begin{pmatrix} -1/4 & 25 \\ 0 & -4 \end{pmatrix}$$

$M_{21} = 0$

TELESCOPE SYSTEM

ANGULAR MAGNIFICATION

MC3



FOR SPATIAL COHERENCE

$$l_c = \frac{\lambda}{\theta} \cdot 1.22$$

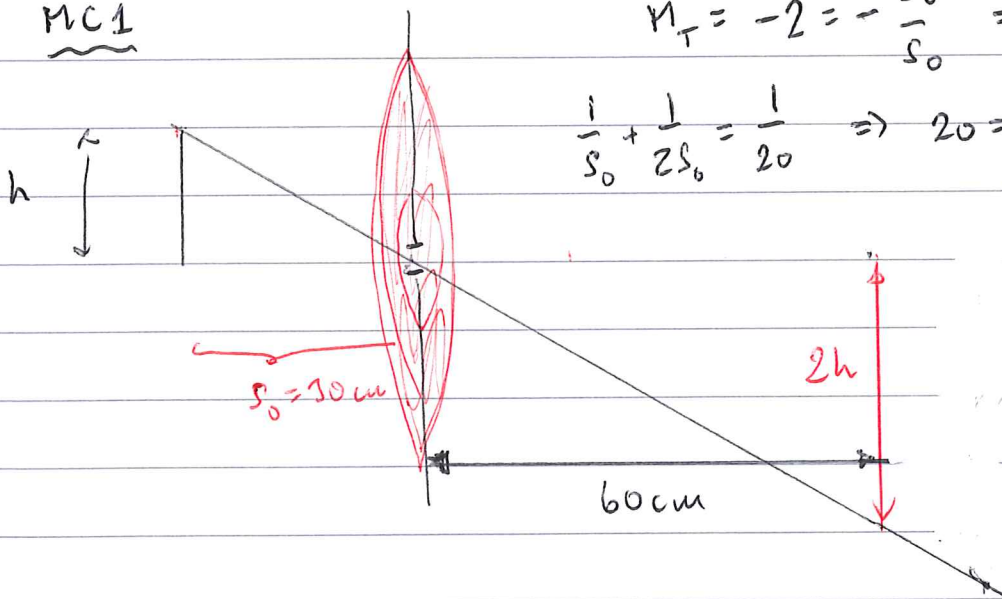
$$\theta \approx \frac{s}{r}$$

CIRCULAR APERTURE

$$\Rightarrow l_c = \frac{550 \cdot 10^{-9} \cdot 0.25 \cdot 1.22}{250 \cdot 10^{-6}} \sim 6.7 \cdot 10^{-4} \text{ m} \sim 0.67 \text{ mm}$$

670 μm

MC1



$$M_T = -2 = -\frac{s_i}{s_o} \Rightarrow s_i = 2s_o$$

$$\frac{1}{s_o} + \frac{1}{2s_o} = \frac{1}{20} \Rightarrow 20 = \frac{2s_o}{3} \Rightarrow s_o = 30 \text{ cm}$$