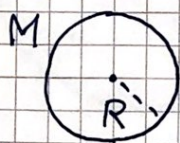


(30)

22.09.21

Beregning av treghetsmoment

Eks 1: Tynn ring / Hul sylinder



$$I_o = \int g^2 dm = R^2 \int dm = \underline{\underline{MR^2}}$$

Eks 2: Ring med en viss tykkelse



"Trik": Tynn ring med radius g (mellom R_i og R_y her) og tykkelse dg har areal $dA = 2\pi g \cdot dg$ (omkrets $\cdot$ tykkelse)

$$\Rightarrow \frac{dm}{M} = \frac{2\pi g dg}{\pi(R_y^2 - R_i^2)}$$

$$\begin{aligned} \Rightarrow I_o &= \int g^2 dm = \int_{R_i}^{R_y} g^2 \cdot M \cdot \frac{2g dg}{R_y^2 - R_i^2} \\ &= \frac{2M}{R_y^2 - R_i^2} \cdot \int_{R_i}^{R_y} \frac{1}{4} g^4 = \underline{\underline{\frac{1}{2} M (R_y^2 + R_i^2)}} \end{aligned}$$

$$(\text{sidan } R_y^4 - R_i^4 = (R_y^2 + R_i^2)(R_y^2 - R_i^2))$$

Ringen på laben:

$$R_y = 25 \text{ mm}, \quad R_i = 22 \text{ mm}$$

$$\Rightarrow I_o \approx 0.89 MR^2 \quad (R = R_y)$$

(31)

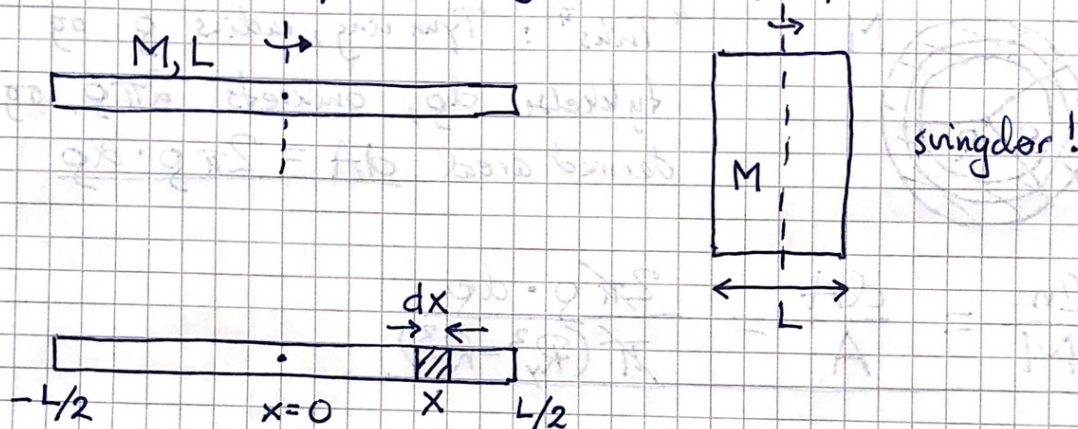
Eks 3: Kompakt skive

= Eks 2 med $R_i \rightarrow 0$

$$\Rightarrow \underline{\underline{I_0 = \frac{1}{2} MR^2}}$$

(og Eks 1 er Eks 2 med $R_i \rightarrow R_y \Rightarrow I_0 = MR^2$)

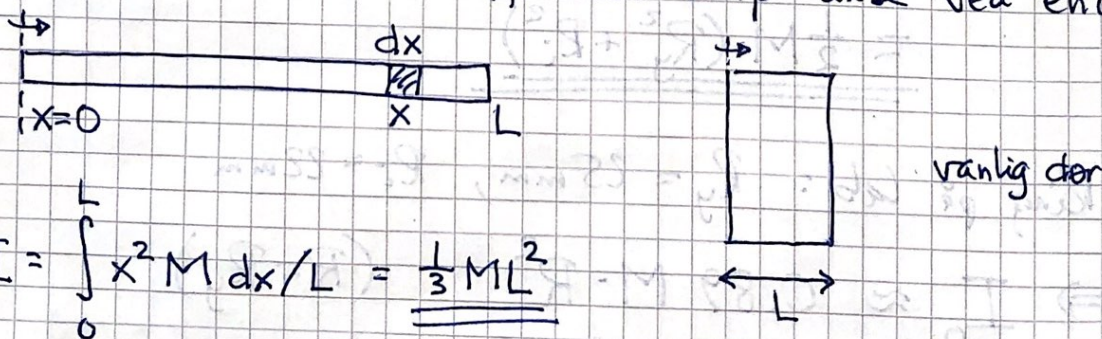
Eks 4: Tynn stang (evt tynn plate, f.eks dør)



$$g \rightarrow x; \quad dm/M = dx/L$$

$$\Rightarrow I_0 = \int_{-L/2}^{L/2} x^2 \cdot \frac{M \cdot dx}{L} = \underline{\underline{\frac{1}{12} ML^2}}$$

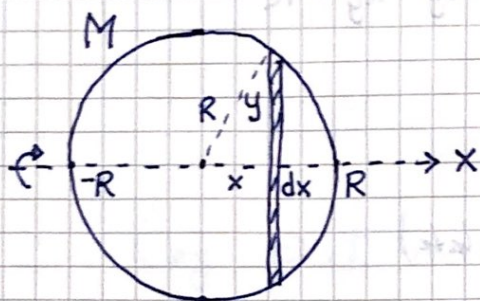
Eks 5: Som Eks 4, men mhp akse ved enden



$$I = \int_0^L x^2 M dx/L = \underline{\underline{\frac{1}{3} ML^2}}$$

(32)

Eks 6: Kompakt kule



= skiver med tykkelse dx ,
 radius $y(x) = \sqrt{R^2 - x^2}$,
 treghetsmoment $dI_0 = \frac{1}{2} \cdot dm \cdot y^2$;
 $-R \leq x \leq R$

$$\frac{dm}{M} = \frac{dV}{V} = \frac{\pi y^2 \cdot dx}{\frac{4}{3}\pi R^3} = \frac{3}{4} \cdot \frac{R^2 - x^2}{R^3} \cdot dx$$

$$\Rightarrow I_0 = \int dI_0 = \int_{-R}^R \frac{1}{2} \cdot M \cdot \frac{3}{4} \cdot \frac{R^2 - x^2}{R^3} \cdot dx \cdot (R^2 - x^2)$$

$$= \frac{3M}{8R^3} \int_{-R}^R (R^4 - 2R^2x^2 + x^4) dx$$

$$= \frac{3M}{8R^3} \cdot \left(R^4x - \frac{2}{3}R^2x^3 + \frac{1}{5}x^5 \right) \Big|_{-R}^R$$

$$= \frac{3M}{8R^3} \cdot R^5 \cdot \left(2 - \frac{4}{3} + \frac{2}{5} \right)$$

$$= MR^2 \cdot \frac{3}{8} \cdot \frac{30 - 20 + 6}{15}$$

$$= \underline{\underline{\frac{2}{5}MR^2}}$$

Eks 7: Tynt kuleskall = ringer med bredde dx ,
 radius $\sqrt{R^2 - x^2}$, treghetsmoment $dI_0 = dm \cdot y^2$, og
 $dm/M = dA/A = 2\pi y \cdot dx / 4\pi R^2 \Rightarrow \underline{\underline{I_0 = \frac{2}{3}MR^2}}$

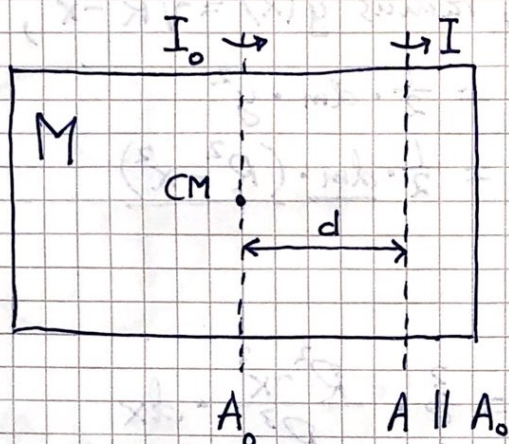
Hit
 22.09.21
 Uke 38

(33)

Steiners sats (Parallellaksesteoremet)

(Uke 39!)

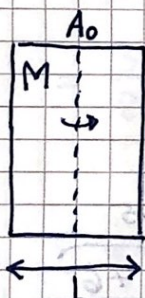
27.09.21



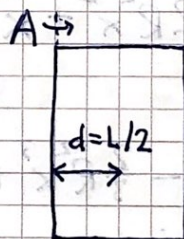
$$I = I_0 + Md^2$$

som gjelder generelt
når aksene A_0 og A
er parallelle

Eks 1: Svingdør vs vanlig dør

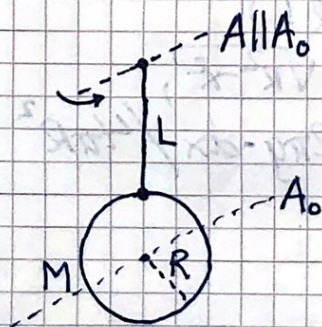


$$I_0 = \frac{1}{12} ML^2$$



$$\begin{aligned} I &= I_0 + Md^2 \\ &= \frac{1}{12} ML^2 + M \cdot \left(\frac{L}{2}\right)^2 \\ &= \underline{\underline{\frac{1}{3} ML^2}} \quad (\text{som s. 31}) \end{aligned}$$

Eks 2: Fulekule i tråd



$$d = R + L$$

 $\Rightarrow$

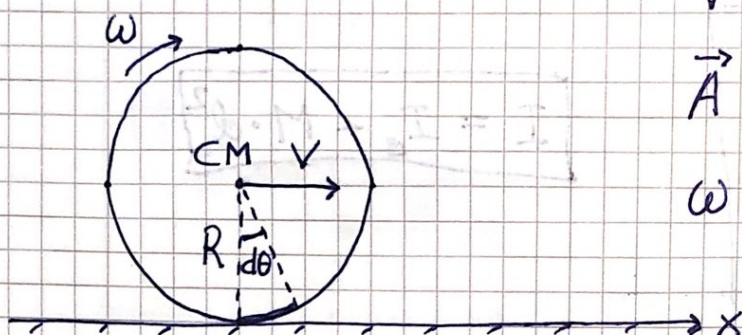
$$\underline{\underline{I = \frac{2}{3} MR^2 + M \cdot (R+L)^2}}$$

$$I_0 = \frac{2}{3} MR^2$$

(kuleskall)

Fysisk pendel; svingetida (perioden)
 T er prop. med $\sqrt{I}$

(34)

Rulling

$$\vec{V} = \frac{d\vec{R}_{cm}}{dt} = \dot{\vec{R}}_{cm}$$

$$\vec{A} = \ddot{\vec{R}}_{cm} = \dot{\vec{V}}$$

$$\omega = \frac{d\theta}{dt}$$

Se på ren rulling (dvs uten å gli).

Når legemet har rotert en liten vinkel $d\theta$ omkring CM, har CM flyttet seg en lengde dx som tilsvarer buelengden $R \cdot d\theta$.

Dermed: $\frac{dx}{dt} = \frac{R \cdot d\theta}{dt} \Rightarrow$

$$\boxed{V = R \cdot \omega}$$

Rullebetingelsen

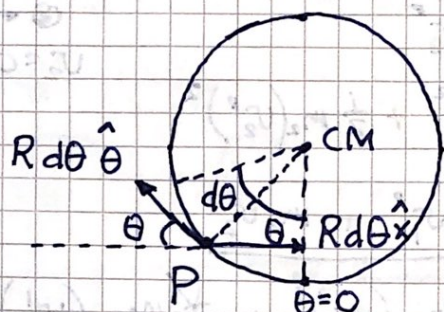
Som i neste omgang gir $A = \frac{dV}{dt} = R \frac{d\omega}{dt} = R \alpha$;

$\alpha = \dot{\omega}$ = vinkelakselerasjonen

$$\boxed{A = R \alpha}$$

er også en rullebetingelse

(35)

Förflyttning $d\vec{r}$ för punkt P på periferien:

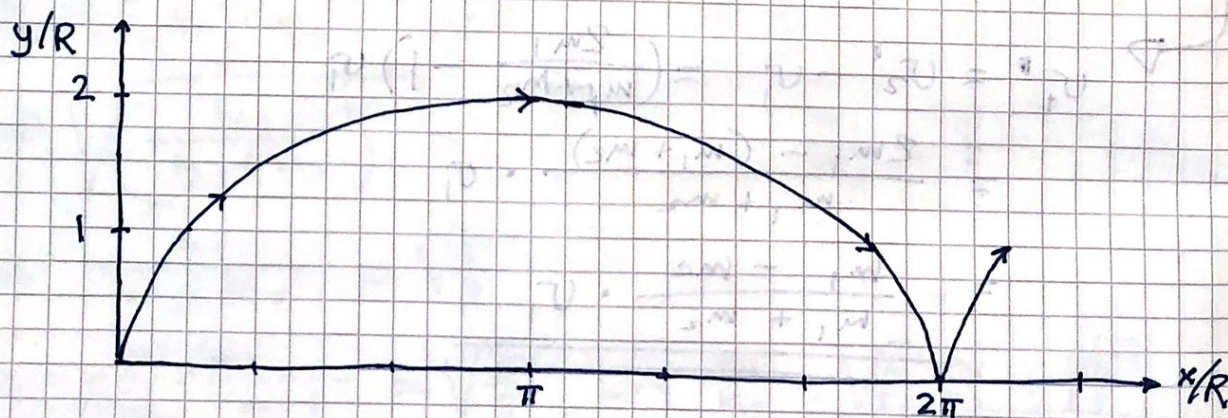
Fra figur:

$$\hat{\theta} = -\hat{x} \cos \theta + \hat{y} \sin \theta$$

$$\begin{aligned} d\vec{r} &= R d\theta \hat{x} + R d\theta \hat{\theta} \\ &= R d\theta (1 - \cos \theta) \hat{x} + R d\theta \sin \theta \hat{y} \end{aligned}$$

$\Rightarrow$ Posisjonen $\vec{r}$ til P, med start i $\vec{r} = (\hat{x}, \hat{y}) = (0, 0)$ när $\theta = 0$:

$$\begin{aligned} \vec{r} &= \int d\vec{r} = \int_0^\theta \{ R d\theta (1 - \cos \theta) \hat{x} + R d\theta \sin \theta \hat{y} \} \\ &= \hat{x} R (\theta - \sin \theta) + \hat{y} R (1 - \cos \theta) \end{aligned}$$

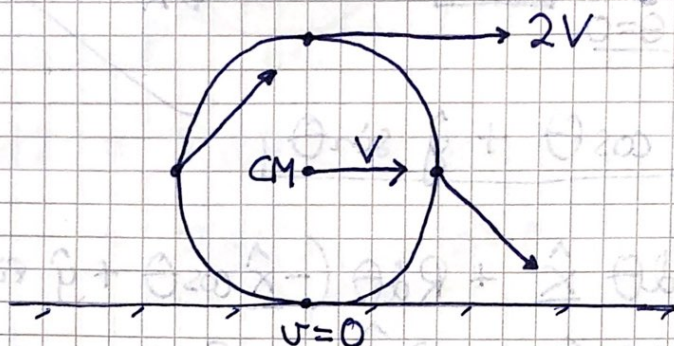


en sykleide

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Farten til P :

$$\begin{aligned}\vec{v} &= \frac{d\vec{r}}{dt} = \hat{x} (R\dot{\theta} - R\dot{\theta} \cos\theta) + \hat{y} R\dot{\theta} \sin\theta \\ &= \hat{x} V (1 - \cos\theta) + \hat{y} V \sin\theta\end{aligned}$$



Når P har kontakt med underlaget, er $v=0$

$\Rightarrow$ Null effekttap pga friksjon:

$$P_f = \vec{f} \cdot \vec{v} = 0 ; \text{ også når } f \neq 0$$

Siden $\omega = V/R$ ved ren rulling, kan vi slå sammen

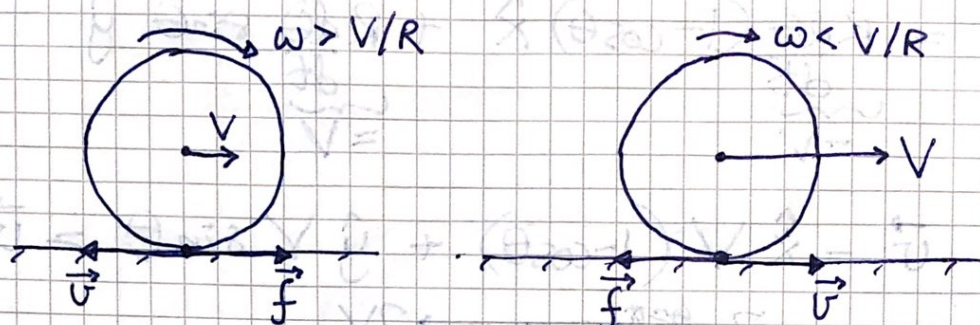
K_{trans} og K_{rot} :

$$\begin{aligned}K &= \frac{1}{2} MV^2 + \frac{1}{2} I_0 \omega^2 = \frac{1}{2} MV^2 + \frac{1}{2} \cdot c MR^2 \cdot \frac{V^2}{R^2} \\ &= \frac{1}{2} (1+c) MV^2\end{aligned}$$

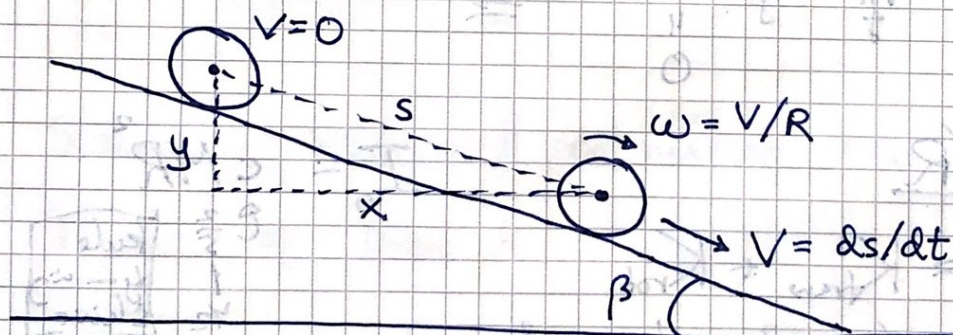
Objekttype	Kompakt kule	Kompakt skive	Kule-skall	Tynn ring
c-verdi	2/5	1/2	2/3	1

(37)

01.10.21

Hvis $\omega \neq V/R$, har kontaktpunktet fart $v = V - \omega R \neq 0$, og legemet slurer (roterer og glir).

$$P_f = \vec{f} \cdot \vec{v} < 0 \quad (f = \mu_k \cdot N; \text{ kinetisk friksjon})$$

Legemer taper mekanisk energi $|P_f|$ pr tidsenhetRen rulling på skråplanFinn V , A og f , samt maksimal β
som gir ren rullingFra sist: Rullebetingelsen: $V = \omega R$

$$K_{\text{rot}} = \frac{1}{2} I_0 \omega^2 = \frac{1}{2} \cdot c M R^2 \cdot \frac{V^2}{R^2} = \frac{c}{2} M V^2$$

(38)

Energibevarelse: $Mgy = \frac{1}{2}(1+c)MV^2$

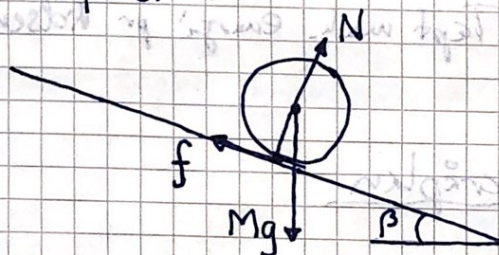
$$\Rightarrow V = \sqrt{\frac{2gy}{1+c}} \quad (y = s \cdot \sin\beta)$$

Akselerasjon:

$$A = \frac{dV}{dt} = \frac{dV}{dy} \frac{dy}{ds} \frac{ds}{dt}$$

$$= \sqrt{\frac{2g}{1+c}} \cdot \frac{1}{2} y^{-1/2} \cdot \sin\beta \cdot V = \frac{g \sin\beta}{1+c}$$

Krefter:



N1 $\perp$ skråplanet $\Rightarrow N = Mg \cos\beta$

N2 $\parallel$ " $\Rightarrow Mg \sin\beta - f = MA$

$$\Rightarrow \underline{f} = Mg \sin\beta - M \cdot \frac{g \sin\beta}{1+c}$$

$$= Mg \sin\beta \left(1 - \frac{1}{1+c}\right) = \frac{c}{1+c} Mg \sin\beta$$

Ren rulling betyr statisk friksjon.

Fra før (30.08.21, s. 11): $f \leq \mu_s \cdot N$

$$\Rightarrow \frac{c}{1+c} Mg \sin\beta \leq \mu_s Mg \cos\beta$$

$$\Rightarrow \underline{\tan\beta \leq \mu_s \cdot \frac{1+c}{c}}$$

39) Plast mot plast og metall mot plast: $\mu_s \approx 0.2 - 0.5$

Eks: Kompakt skive, $c = 1/2$; $\mu_s = 0.2$

$$\tan \beta \leq 0.2 \cdot \frac{1+0.5}{0.5} = 0.6$$

$$\Rightarrow \beta \leq \arctan 0.6 = 31^\circ$$

Ren rulling på berg-og-dal-bane

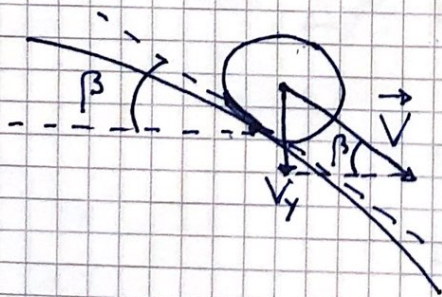
Varierende helningsvinkel β ; kan ha rulling både oppover og nedover; banen krummer oppover og nedover.

Energibevarelse gir

$$V = \sqrt{\frac{2gy}{1+c}}$$

$$\text{og } A_{||} = \frac{g \sin \beta}{1+c}$$

som med skråplan:



$$A_{||} = \frac{dV}{dt} = \sqrt{\frac{2g}{1+c}} \cdot \frac{1}{2} y^{-1/2} \cdot \frac{dy}{dt}$$

$$\frac{dy}{dt} = V_y = V \sin \beta = \sqrt{\frac{2gy}{1+c}} \sin \beta$$

$$\Rightarrow A_{||} = \frac{g \sin \beta}{1+c}$$

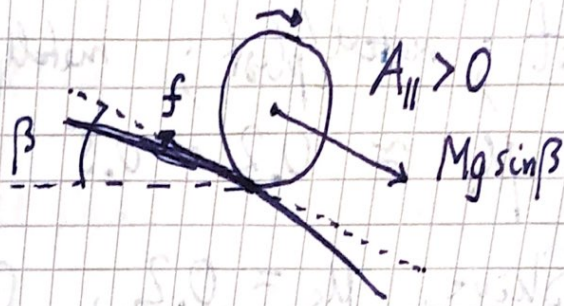
$$N \perp \text{ banen} : Mg \sin \beta - f = MA_{||}$$

$$\Rightarrow f = \frac{c}{1+c} Mg \sin \beta ; \text{ som skråplan}$$

(40)

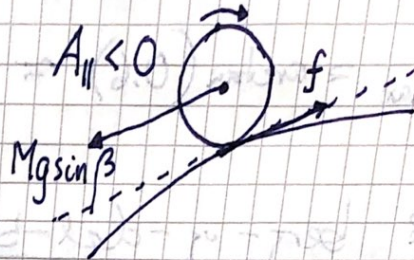
Nedover:

$$\beta > 0$$



Oppover:

$$\beta < 0$$



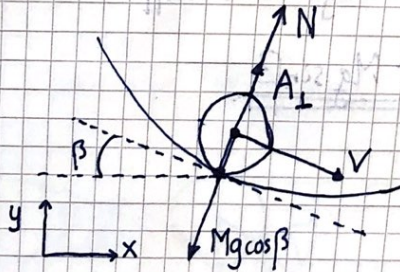
$N \perp$ banen: $\sum F_{\perp} = MA_{\perp}$; $A_{\perp} = \frac{V^2}{\rho}$

ρ = banens krumningsradius

$$= [1 + (y')^2]^{3/2} / |y''|$$

Krumning oppover: $y'' > 0$ (når y øker oppover)

$$y' = \frac{dy}{dx} = -\tan \beta \quad (\beta > 0)$$



$$\sum F_{\perp} = N - Mg \cos \beta$$

$$A_{\perp} = V^2 / \rho > 0$$

$$V^2 = \frac{2gy}{1+c}; \quad y = \text{høydeendring fra startpos. } (y > 0)$$

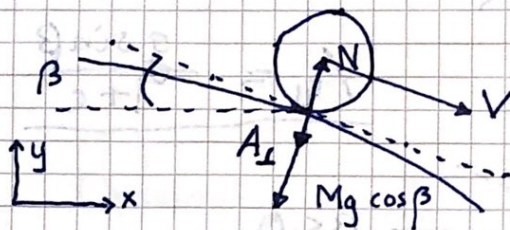
$$N = MA_{\perp} + Mg \cos \beta = MV^2 / \rho + Mg \cos \beta$$

$$= M \cdot \frac{2gy}{1+c} \cdot \frac{y''}{[1+(y')^2]^{3/2}} + Mg \cos \beta$$

(41)

Krumning nedover: $y'' < 0$

$$y' = -\tan \beta$$



$$MA_{\perp} = Mg \cos \beta - N$$

$$\Rightarrow N = Mg \cos \beta - MA_{\perp} = Mg \cos \beta - M \frac{V^2}{|g|}$$

$$= Mg \cos \beta - M \cdot \frac{2gy}{1+c} \cdot \frac{|y''|}{[1+(y')^2]^{3/2}}$$

For å ha ren rulling må vi også her ha en statisk friksjonskraft

$$f \leq \mu_s \cdot N,$$

dvs

$$\mu_s \cdot N \geq \frac{c}{1+c} Mg \sin \beta$$

Dvs: Normalkraften N fra banen må hele veien være tilstrekkelig stor, slik at ulikheten

$$f/N \leq \mu_s$$

er oppfylt. Vi ser at stor fart V og krumning nedover bidrar til at N kan bli (for?) liten.